

Design of Dilute Phase Pneumatic Conveying

Product : **flour** pressure drop across jet filter : 10 mbar : 0.1 psi

mat'l of pipe : **stainless steel**

mass product flo : **6,000** kg/h : 13,228 lbm/h pressure drop across blower inlet & silencer : **450** mbar : 6.6 psi

this value control final air velocity

partic e size	mm	B.D (kg/ m3)	Ut(m/ s)	pipe roughness	k=m m
flour	0.02	0.6	4.64	stainless steel	0.02
sugar	0.5	0.9	4.405	carbon steel	0.05
talc	0.01				
HDPE	4	946	9.32		

Ambient temp. : **25** °C : 85 °F conveying distance
 Ambient pressure: **1.013** bar : 14.8911 psi horizontal : **15** m : 49 ft
 particle size : 0.02 mm : 6.6E-05 ft horizontal : **15** m : 49 ft horizontal 2 has acceleration zone
 clean air line : **85** mm : 3.34646 inch vertical : **0** m : 0 ft
 B.D of product : 0.6 kg/m3 : 0.03746 lbm/ft3 bend : **4** ea
 pipe roughness : 0.02 mm : 6.6E-05 ft
 bend radius >= : 765 mm
 R/D >= 6 ~ 12 : 9
 mass air flow : 516 Nm3/h : 304 SCFM : **8.60** m3/min
 velocity mat'l, Ut : 4.6 m/s 15.2 ft/s

Gas density at point "jet filter" from ideal gas law : 0.074 lbm/ft3 : 1.183 kg/m3
 Solid mass to air mass ratio=constant : 9.8 (Generally sugar:4.9, flour:9.8)

Components sum to total Pressure drop

1. jet filter : 15.04 psi : 1.02 bar

2. Horizontal 1 : 0.7646 psi : 0.05 bar

A : 0.0611 ft2 ρ_g : 0.075 lbm/ft3 : 1.195 kg/m3

Vg1 : 82.14 ft/s : 25.0 m/s

μ_g : 0.0000114 lbm/ft.s

Re: 149,980

Dynamic viscosity of air (0 deg.) = $1.74 \times 10^{-6} = 0.0174$ cP, 1cP=6.72 x 10⁻⁴ lbm/(ft.s)

Dynamic viscosity of air (15 deg.) = $1.78 \times 10^{-6} = 0.0178$ cP

Dynamic viscosity of air (0 deg.) = $1.79 \times 10^{-6} = 0.0179$ cP

A : 1.48847E+21

B : 2.36333E-10

Gas friction factor from Churchill's equation, f : 0.005

$F_{r=constant}$: 14.4056 Fr : 752

Solids Friction Factor, $\lambda z=constant$: 0.006

4. Bend : 16.98 psi : 1.15 bar

Vg3 : 71.82 ft/s : 21.9 m/s

ρ_g : 0.084 lbm/ft3 : 1.349 kg/m3

5. Vertical : 16.978 psi : 1.15 bar

Vg4 : 71.82 ft/s : 21.9 m/s

Vg1	82.14
Vg3	71.82
Vg4	71.82
Vg5	68.52

Fr : 574.9 ρ_g : 0.084 lbm/ft³ : 1.349 kg/m³

$\lambda z = \text{constant}$: 0.008

V_p / V_g : 0.9987 V_p : 71.73 ft/s ϵ : -21.39 ρ^0 : -1 lbm/ft³
0 0 (ϵ :Void fraction of gas phase, ρ^0 :Bulk density)

6. Horizontal 2 : 17.91 psi : 0.05 bar ρ_g : 0.089 lbm/ft³ : 1.432 kg/m³

ΔP_{accel} : 0.9338 psi **Vg5 : 68.52 ft/s : 20.9 m/s**

ΔP_{horiz} : 0.8174 psi Fr : 574.9

$\lambda z = \text{constant}$: 0.008

P_g^1 : 17.80 psi

P_g : 17.91 psi

Pressure Drop Across Blower

Inlet pressure to blower P_{in} : 8.085 psi : 0.55 bar

ΔP_{blower} : **9.83 psi : 0.67 bar** 668 mbar 6,817 kg/m²

This is the pressure increase required by the blower.

Electric power of blower : 13.68 kw

Check Saltation Velocity

Use the Rizk Correlation V_{gs} : 53.846 ft/s : 16.4 m/s

δ : 1.9888 χ : 2.522

From the Rizk equation, the largest saltation velocity occurs at the smallest gas density. (at the jet filter)

The smallest velocity(V_g) : 68.52 ft/s 28.61 m/s

Result

1 The conveying gas velocity is O.K

2 The blower pressure must be increased by ΔP_{blower}

Note : The conveying gas velocity(V_g) is generally equal to or above the saltation velocity(V_{gs}) of the material being conveyed at the dilute phase conveying System.